





AIR BUBBLER SYSTEM DESIGN FOR THE 140-FOOT WYTM



JANUARY 1976



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NAVAL ENGINEERING DIVISION WASHINGTON, D.C. 20593

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AIR BUBBLER
SYSTEM DESIGN
FOR THE 140-FOOT WYTM

Ву

E.J. Lecourt

January 1976

FINAL REPORT

CONTRACT NO. DOT-CG-50383-A

Prepared for

Department of Transportation United States Coast Guard Office of Engineering 400 Seventh Street, S.W. Washington, D.C. 20590

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NOMENCLATURE

d = manifold diameter

f = friction coefficient

t = manifold length between orifices

q = flow rate from orifice

 A_0 = orifice area

 c_D = discharge coefficient

K = manifold flow coefficient

 Q_1 = flow rate approaching orifice location

 V_1 = fluid velocity approaching orifice location

 ΔP = change in pressure

 ΔP_0 = pressure differential across orifice

 ρ = mass density

I. DESCRIPTION OF THE SYSTEM

The air bubbler system designed for the 140-foot WYTM consists of four manifolds, an air compressor driven by a diesel engine, and the necessary piping and valves.

The two forward or bow manifolds consist of two 6" x 4" rectangular tubes which are located on the center line below the molded keel line from the forefoot at about Frame 9 to Bulkhead 32. Six Grifices are located in the outboard side of each tube. The location and the size of each orifice is listed in Table I.

The two aft manifolds consist of two air ducts located within the hull, outboard of the 9' Buttock, and extending from Bulkhead 32 to Bulkhead 61. The width of the duct is 8 inches and the height of the inboard side is approximately 8 inches. The hull plating forms the bottom of the duct. The dimensions of the inboard and outboard sides of the duct vary with the slope of the hull. These manifolds each have eight orifices through the hull plating; the location and size of each orifice is listed in Table II.

The spacing of the orifices in the manifolds described above is 6 feet. An alternate design with orifices located every 4-1/2 feet was also prepared. The number, size, and location of the orifices for these alternate manifolds are listed in Tables A-1 and A-2 of Appendix A.

The air for the bubbler system is supplied by an air compressor with a capacity of 7500 SCFM at 9 psig. The compressor will be driven by a diesel engine rated at 350 HP. The diesel-compressor will be located in a van on the main deck above the motor room.

The piping system consists of a 12" main which divides in the engineroom into two 10" mains. The branches to each manifold are 8" pipe. A schematic of the piping system is shown in Figure 1.

In each branch, a straight run has been provided with fittings for a flowmeter, pressure gage, and thermometer. These will be utilized for installing instruments for testing the effectiveness of the bubbler system.

The design of the system provides four modes of operation:

- 1. all four manifolds
- 2. two bow manifolds only
- 3. two starboard side manifolds only
- 4. two port side manifolds only.

Motor operated butterfly valves are located at each manifold to permit changing the mode of operation.

The first mode is the normal mode for operations in ice. The second mode allows all of the air to be supplied to the bow manifolds if this should prove to be more effective. The third and fourth modes are for maneuvering in restricted waters, providing the capability of moving the bow to the right or left. The characteristics of the system for each mode of operation are explained in the following section.

TABLE I.

FORWARD MANIFOLDS, PORT AND STARBOARD
6-FOOT ORIFICE SPACING

| Location (Frame No.) | Diameter (inches) |
|----------------------|--|
| 10 - 11 | 1.875 |
| 14 - 15 | 1.875 |
| 18 - 19 | 2.000 |
| 22 - 23 | 2.000 |
| 26 - 27 | 2.125 |
| 30 - 31 | 2.125 |
| | (Frame No.) 10 - 11 14 - 15 18 - 19 22 - 23 26 - 27 |

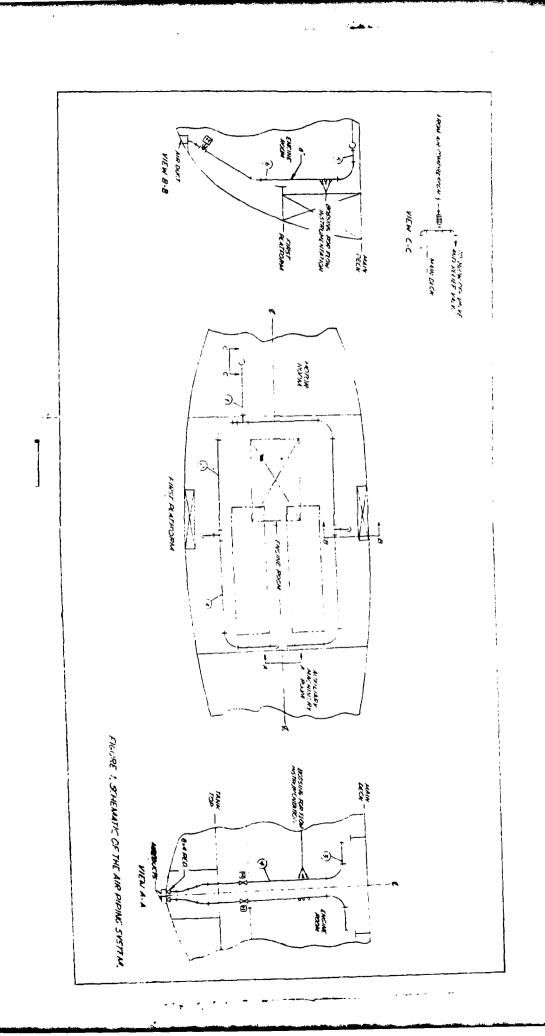
SUPPLY AT AFT END OF MANIFOLD.

TABLE II.

AFT MANIFOLDS, PORT AND STARBOARD
6-FOOT ORIFICE SPACING

| Orifice No. | Location (Frame No.) | Diameter (inches) |
|-------------|----------------------|----------------------|
| 1 | 32 - 33 | 1.438 |
| 2 | 36 - 37 | 1.562 |
| 3 | 40 - 41 | 1.562 |
| 4 | 44 - 45 | 1.562 |
| 5 | 48 - 49 | 1.562 |
| 6 | 52 ~ 53 | 1.562 |
| 7 | 56 ~ 57 | 1.562 |
| 8 | 60 - 61 | 1.438 |
| | | |

SUPPLY BETWEEN ORIFICES NO. 4 AND 5.



II. OPERATING CHARACTERISTICS

The characteristics of the air bubbler system for each mode of operation are summarized in Table III. The air flow and pressure at the compressor are determined by the characteristics of the compressor, the piping system, and the manifolds.

Typical compressor characteristics are shown in Figures 2 and 3. Air flow versus discharge pressure is shown in Figure 2, and power versus discharge pressure is shown in Figure 3. The operating pressure of the system is limited by the power of the diesel engine.

The air flow through each orifice is a function of the pressure in the manifold, the hydrostatic pressure outside the manifold, and the diameter of the orifice. Calculations have been performed to determine the air flow characteristic versus manifold pressure, and the results are presented in graphical form in Figures 4, 5, 6, 7, and 8. A computer program was used to perform the calculation, and the printout is included in Appendix B.

The pressure drop in the piping system has been calculated for each mode of operation and is tabulated in Table III.

In modes 3 and 4, the total air flow cannot be supplied to the manifolds on one side of the ship without exceeding the 9 psig pressure limit imposed by the torque limit of the diesel engine. It is, therefore, necessary to provide a blow-off of 750 SCFM through a special valve in order to keep the pressure at 9 psig.

The characteristics of the alternate manifolds with 4-1/2-foot spacing are almost identical. Graphs of the characteristics are included in Appendix A, and the supporting calculations are included in Appendix B.

TABLE III OPERATING CHARACTERISTICS FOR EACH MODE

| MODE | | AII (S | FLO CFM | ow) | | PR (F | ESSURE SIG) | - | POWER (HP) |
|------|---------------------------|---------------------------|---------------------------|---------------------------|----------------|--------------|----------------|----------------|---------------|
| | Bow Marifold Stod Side | Bow Hanifold Port Side | Aft Manifold Stod Side | Aft Wanifold Port Side | Total Air Flow | Bow Manifold | Aff Namifold | Air Compressor | Diesel Engine |
| 1. | 1700 | 1700 | 2050 | 2050 | 7500 | 5.7 | 5.7 | 6.4 | 250 |
| 2. | <i>3750</i> | 3750 | | - | 7500 | 7.8 | | 9.0 | 325 |
| . 3. | <i>3550</i> | - | 3200 | - | 6750 | 7.5 | 7.7 | 8.9 | 325 |
| 4. | - | 3550 | _ | 320 0 | 6750° | 7.5 | 7.7 | 8.9 | 325 |

^{*} Blow-off required equal to 750 scfm

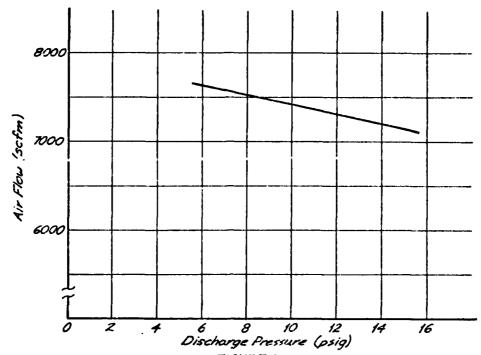


FIGURE Z AIR FLOW VS DISCHARGE PRESSURE FOR INGERSOLL-RAND TYPE L AXX 178 x Z8 COMPRESSOR AT 1710 RPM

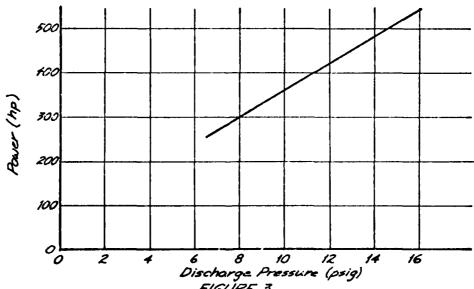


FIGURE 3
POWER VS DISCHARGE PRESSURE
FOR INGERSOLL-RAND TYPE L AXX 138 x 28 COMPRESSOR AT 1770 RPM

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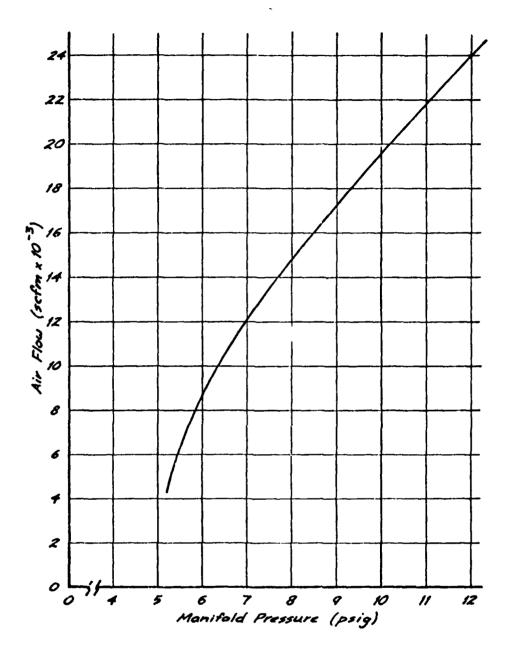


FIGURE 4
AIR FLOW CHARACTERISTIC WITH ALL MANIFOLDS

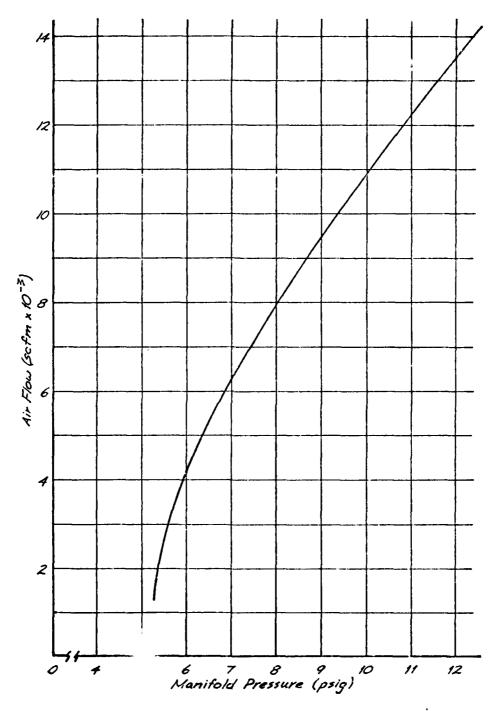


FIGURE 5 AIR FLOW CHARACTERISTIC WITH TWO BOW MANIFOLDS

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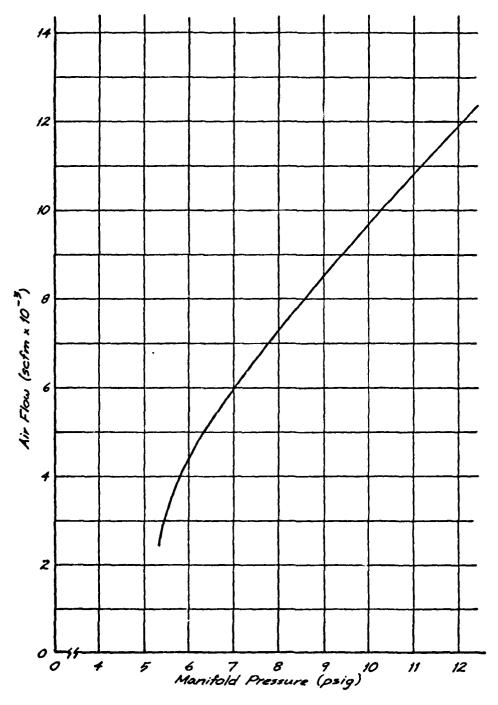


FIGURE 6
AIR FLOW CHARACTERISTIC WITH PORT OR STARBOARD MANIFOLDS

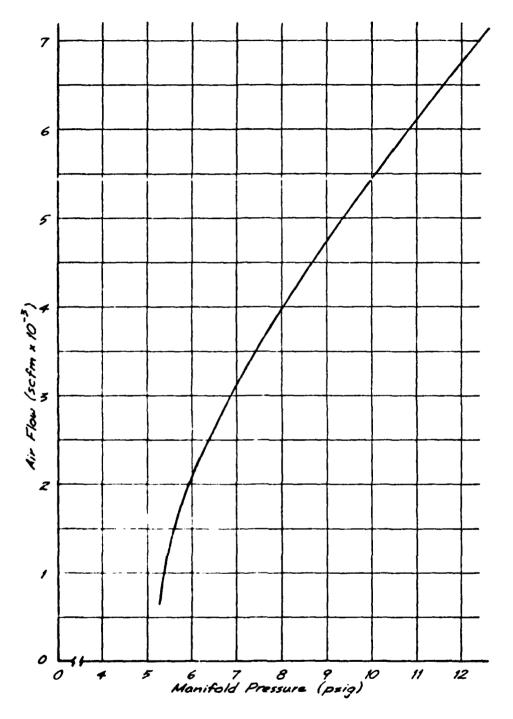


FIGURE 7
AIR FLOW CHARACTERISTIC OF ONE BOW MANIFOLD

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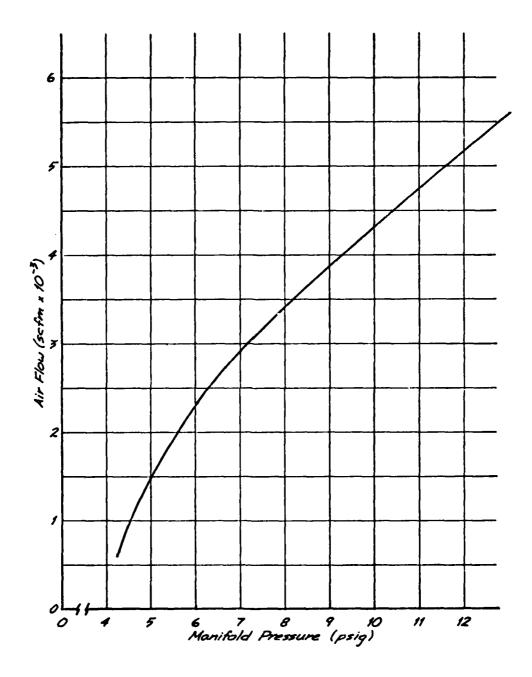


FIGURE 8 AIR FLOW CHARACTERISTIC OF ONE AFT MANIFOLD

III. DESIGN HISTORY

System Capacity

The only published data of operating experience with air bubbler systems has been from two experimental programs. The first was the U.S. Coast Guard testing program with the USCGC SUNDEW and the second was the MARAD testing program with the SS LEON FRASER (Reference 1). Neither program resulted in a specific criterion for establishing the capacity of a system; however, engineering judgement has led to a rule-of-thumb which sets the minimum capacity as one SCFS per foot of ship covered by the manifolds. The manifolds on the WYTM will extend for about 80 feet of the length of the ship. Using this rule-of-thumb, the minimum capacity would be approximately 5000 SCFM.

Other factors which must be considered are the operating pressure of the system, the capacity of air compressors available, and the ratings of diesel engines which are candidates as prime movers. Taking these factors into consideration and allowing a margin for test purposes, the system capacity was set at 7500 SCFM at 9 psig with a prime mover of 350 HP.

Size and Spacing of Orifices

The air flow rate, system pressure, and the size and spacing of the orifices are all interrelated. To solve this problem, two computer programs are available. The first determines the orifice diameter for a given flow rate, and the second calculates the flow rate for a manifold with given orifice diameters.

The programs are written utilizing three fundamental equations. The flow through an orifice is calculated using the following relationship:

$$q = C_D A_0 \sqrt{\frac{2}{\rho} \Delta P_0}$$
 (1)

The pressure at any point in the manifold is a function of friction losses and head gain due to reduced velocities in the manifold between orifices (References 2 and 3). The equation for friction loss is:

$$\Delta P$$
 friction = $f \frac{\rho \mathcal{I} V_1^2}{2d}$ (2)

and the equation for the head increase due to deceleration is:

$$\Delta P$$
 deceleration = $\frac{\rho}{2} V_1^2 \left[2 \frac{q}{Q_1} - (1 + K) \times \left(\frac{q}{Q_1} \right)^2 \right]$ (3)

Starting at the dead end of the manifold and working towards the supply end, the flow at each orifice is calculated knowing the pressure in the manifold at that orifice and the hydrostatic pressure outside the manifold at that orifice. Summing the flows from each orifice gives the total flow, and the pressure at the last orifice is the supply pressure.

Initial investigations for this design considered orifice spacing of 1, 2, 6, and 10 feet. The spacing on the SUNDEW was 12, 14-1/2, and 16 inches, depending on the manifold location. The spacing on the LEON FRASER was every 2 feet, and this spacing resulted in a very uniform distribution. Greater spacing on the WYTM was considered to reduce the number of orifices. Calculations for spacing of 4-1/2 feet and 6 feet were performed in the final design stages. The results of these calculations are in Appendix B. Orifice spacing of 6 feet was the final selection for the WYTM.

The manifold pressure is a function of the total orifice area. Small orifices with higher manifold pressures result in a very uniform flow distribution which is not very sensitive to changes in pressure; however, this requires more horsepower to achieve a given flow rate. In this design for the WYTM a large, total orifice area was utilized to keep the compressor power requirements within limits.

Piping System Design

For analysis of the pressure drop in the air piping system, the system was divided into the six sections listed in Table IV and indicated in Figure 1. Air flow calculations were performed for each mode of operation with the results tabulated in Tables V, VI, and VII. An absolute roughness of .005 feet for galvanized pipe was used in all of the calculations.

TABLE IV
AIR PIPING SYSTEM DESCRIPTION

| Section | | I.D. | Length | ······································ | |
|---------|-------------|----------|--------|--|----------------|
| No. | Description | (inches) | (feet) | Fittings | L/D |
| 1 | 12" SCH 40 | 12.00 | 16 | TEE (branch) ELL (LR) | 60 20 |
| 2 | 10" SCH 40 | 10.02 | 30 | TEE (branch) ELL (LR) | 60 20 |
| 3 | 8" SCH 40 | 7.981 | 30 | TEE (run) ELL (LR) ELL (LR) | 20 20 20 |
| 4 | 8" SCH 80 | 7.625 | 15 | 45° ELL 45° ELL Butterfly Valve | 16 16 20 |
| 5 | 8" SCH 40 | 7.981 | 2 | TEE (branch) ELL (LR) | 60 |
| 6 | 8" SCH 80 | 7.625 | 16 | 45° ELL 45° ELL Butterfly Valve | 16 16 20 |

TABLE V

PRESSURE DROP IN PIPING FOR MODE 1 OPERATION

| Section No. | Air Flow (SCFM) | Air Temp. (°F) | Pressure (psig) | ΔP (psig) |
|----------------|--------------------|-------------------|--------------------|--------------|
| 1 | 7500 | 180 | 6 | .28 |
| 2 | 3750 | 180 | 6 | .18 |
| 3 | 1700 | 180 | 6 | .10 |
| 4 | 1700 | 120 | 6 | .08 |
| 5 | 2050 | 180 | 6 | .10 |
| 6 | 2050 | 120 | 6 | .11 |

TABLE VI
PRESSURE DROP IN PIPING FOR MODE 2 OPERATION

| Section No. | Air Flow (SCFM) | Air Temp. (°F) | Pressure (psig) | ΔP (psig) |
|----------------|--------------------|-------------------|--------------------|--------------|
| 1 | 7500 | 180 | 9 | .26 |
| 2 | 3750 | 180 | 9 | .18 |
| 3 | 3750 | 180 | 9 | .41 |
| 4 | 3750 | 120 | 8 | . 34 |

TABLE VII

PRESSURE DROP IN PIPING FOR MODE 3 AND 4 OPERATION

| Section No. | Air Flow (SCFM) | Air Temp. (°F) | Pressure (psig) | ΔP (ps ig) |
|----------------|--------------------|-------------------|--------------------|-----------------------|
| 1 | 6750 | 180 | 9 | .21 |
| 2 | 6750 | 180 | 9 | .56 |
| 3 | 3550 | 180 | 9 | .37 |
| 4 | 3550 | 120 | 9 | .30 |
| 5 | 3200 | 180 | 9 | .21 |
| 6 | 3200 | 120 | 8 | .25 |

REFERENCES

- Levine, G.H., Voelker, R.P., Mentz, P.B., "Advances in the Development of Commercial Ice-Transiting Ships," SNAME Transactions, Volume 82, 1974.
- 2. Keller, J.D., "The Manifold Problem," Journal of Applied Mechanics, March, 1949.
- 3. McNown, J.S., "Mechanics of Manifold Flow," Trans. ASCE, 1953.

APPENDIX A

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| Table A-1 | Alternate Forward Manifolds, Port and Starboard, 4-1/2-Foot Spacing | A-3 |
| Table A-2 | Alternate Aft Manifolds, Port and Starboard, 4-1/2-Foot Spacing | A-3 |
| Figure A-1 | Alternate Bow Manifold Air Flow Charac- teristic | A-4 |
| Figure A-2 | Alternate Aft Manifold Air Flow Charac- teristic | A-5 |

TABLE A-1.

ALTERNATE FORWARD MANIFOLDS, PORT AND STARBOARD

4-1/2-FOOT ORIFICE SPACING

| Orifice No. | Location (Frame No.) | Diameter (inches) |
|----------------|----------------------|----------------------|
| 1 | 10 - 11 | 1.750 |
| 2 | 13 - 14 | 1.750 |
| ´ 3 | 16 - 17 | 1.750 |
| 4 | 19 - 20 | 1.875 |
| 5 | 22 - 23 | 1.875 |
| 6 | 25 - 28 | 1.875 |
| 7 | 28 - 29 | 1.875 |

SUPPLY AT AFT END OF MANIFOLD.

TABLE A-2.

ALTERNATE AFT MANIFOLDS, PORT AND STARBOARD

4-1/2-FOOT ORIFICE SPACING

| Orifice No. | Location (Frame No.) | Diameter (inches) |
|----------------|----------------------|----------------------|
| 1 | 32 - 33 | 1.315 |
| 2 | 35 - 36 | 1.438 |
| 3 | 38 - 39 | 1.438 |
| 4 | 41 - 42 | 1.438 |
| 5 | 44 - 45 | 1.438 |
| 6 | 47 - 48 | 1.438 |
| 7 | 50 - 51 | 1.438 |
| 8 | 53 - 54 | 1.438 |
| 9 | 56 - 57 | 1.438 |
| 10 | 59 - 60 | 1.315 |

SUPPLY BETWEEN ORIFICES NO. 5 AND 6.

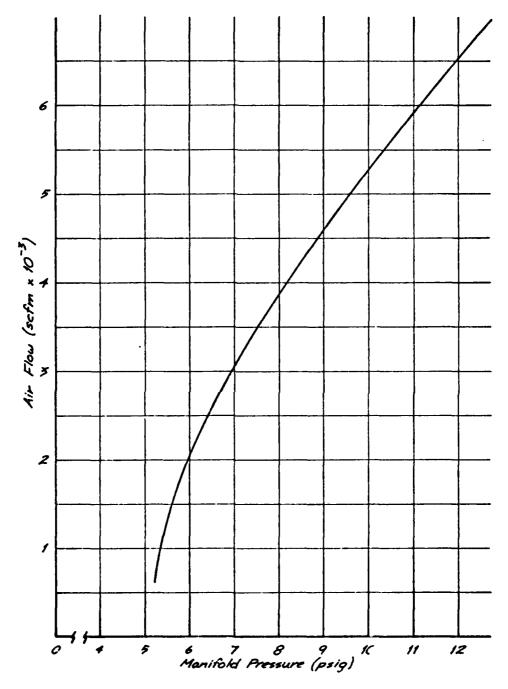


FIGURE A-1 ALTERNATE BOW MANIFOLD AIR FLOW CHARACTERISTIC

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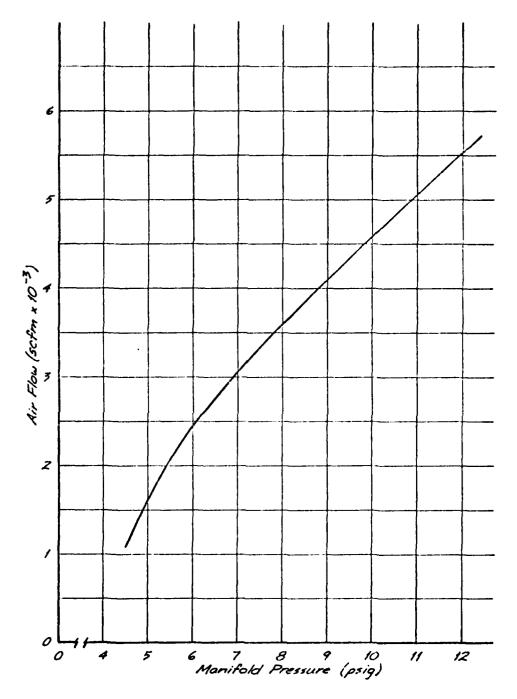


FIGURE A-2 ALTERNATE AFT MANIFOLD AIR FLOW CHARACTERISTIC

APPENDIX B

| | | Page No. |
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TABLE B-1 FORWARD MANIFOLD, 6- FOOT ORIFICE SPACING

| CALCULATION OF MANIFOLD FLOW | FLDM | めた (大学 大の |
|--|---|---|
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| SUPPLY AT DRIFICS 6 | | |
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TABLE B-1 (continued)

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TABLE B-1 (continued)

| F1 P3 AIP DEN F FACT REYND. MAL (PSI) (PLUG/FI3) | 000 7.883 5.113 0.00362 0.0194 0.145E 06 844 7.821 5.113 0.00361 0.0182 0.287E 06 897 7.118 5.113 0.00359 0.0177 0.444E 06 448 7.009 5.156 0.00358 0.0174 0.593E 06 224 6.887 5.200 0.00356 0.0172 0.753E 06 913 6.801 5.200 0.00354 0.0172 0.908E 06 | 13.82 SCFM | P1 P3 RIR DEN F FROT REY NO. (PSI) (PSI) (SLUG/FI3) | 1000 8.275 5.113 0.00378 0.0130 0.173E 05 0538 8.185 5.113 0.00377 0.0179 0.354E 06 0579 8.034 5.113 0.00375 0.0175 0.547E 06 0544 7.873 5.156 0.00378 0.0173 0.730E 06 0544 7.691 5.200 0.00369 0.0172 0.966E 06 0524 7.560 5.200 0.00367 0.0172 0.966E 06 0524 7.560 5.200 0.00367 0.0171 0.118E 07 |
|---|--|------------|--|---|
| PS NDSMAL | 000.00 000.00 000.00 0000.00 00000 00000 00000 00000 | 2913.82 | 03 NDRMAL | |
| 03 SCFS | // 00000 MM 6.000 MM 1000 MM 1000 M | 70 | CSCFS) | 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 |
| V1 (FP⊗ | 44, 74, 74, 74, 74, 74, 74, 74, 75, 75, 75, 75, 75, 75, 75, 75, 75, 75 | AIR FL | V1 (FPS) | |
| DEI NO. | ಈಯಣಕಕ್ಕ | TOT ĤL | 25 25 1 | ⊶0,0, 4 l 0 u |

TABLE B-1 (continued)

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| REV MO. | 000000 000000 | | BEY MO. | 0.000000000000000000000000000000000000 |
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| ίL ίL | 000000 000000 000000 0000000 00000000 | | 田田田 田田田田田田田田田田田田田田田田田田田田田田田田田田田田田田田田田田 | 0000000 000000 000000 00000 |
| PIR DEN (CLUS/RT3) | ကျောက္တာတာတယ္တ တေတာ့တာလုပ္လိုင္ တက္တာလုပ္လိုင္ တည္ဆည္သည္ သည္သည္ သည္သည္ | | AIR DEN VELUGYETS) | 0.00411 0.00409 0.00409 0.00409 0.00000 |
| ⊕ 00.60 | ကက္ကတ္သင္ ဆဆ္ဆက္သင္ ဆည္ဆက္တိုင္း အက္က်က္က်က္ကို | | 0 0 0 0 0 | |
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| TEMACH CO | | 49.09. 49.09. | 14880% 80 | |
| 63 (80F3) | | : E | 00 00 00 00 00 00 00 00 00 00 00 00 00 | |
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| REY NO. | 0.00.00 0.00.00 0.00.00 0.11078 0.000 0.000 0.000 | |
| F FACT | 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0 | |
| AIR DEN (SLUG/FT3) | 0.00488 0.00488 0.00488 0.00488 0.00488 | |
| 88 0 0 | | |
| P1 (PSI) | 1111 1111 1111 1111 1111 1111 1111 1111 1111 | E () () |
| O3 NDRMAL | | ្រ ក្ ក្ ក្ ក្ |
| 03 (SCFS) | 14.00.00 10.7660 14.00.44 10.7600 10.21000 | FLOW |
| V1 (FPS) | 27 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 | AIR |
| HE I | ⇔ಹಣ್ಣಕ⊩್ಯ | TOTAL |

| | 4440000 000000 |
|-----------------------|---|
| REY NO. | 0.091 0.093 0.087 0.117 0.117 0.148 0.148 0.148 0.148 0.148 0.148 |
| F FACT | 0.0188 0.0178 0.0178 0.0178 0.0170 |
| AIR DEN (SLUGZFT3) | 0.000.00 0.000.00 0.0000.00 0.0000000 0.000000 |
| 0 0 0 0 | សូសូត្រូស្ត 1111 1111 1111 1111 1111 1111 1111 1 |
| E E E | 4 0 0 0 0 0 0 4 4 0 0 0 0 0 0 0 1 0 0 0 0 0 1 0 0 0 |
| OB NDRMAL | 1.0000 1.0000 1.0000 1.0000 1.10000 1.0000 1.0000 |
| 03 (SCFS) | |
| V1 (FPS) | 24.00.00 24.00.00 24.00.00 26.00.00 26.00.00 26.00.00 |
| 180 100 100 | ⇔ល្យ±ស្ចេ |

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| V1 GPP | 0000000 0000000 0000000 0000000 0000000 |
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TOTAL AIP FLOW

TABLE B-2 AFT MANIFOLD, 6-FOOT ORIFICE SPACING, ORIFICES NO. 1-4

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| \$2.79.78 | | | ⊢ L | SO IN | | DEGREES F SLUG3/FT-SEC+19000 PSI/FT | |
|------------------------------|-----------------------------|---------------------|---|---|--|---|--|
| FLOW | TERS | ٠ | 4.0 0.620 | 18.0 37.7 5.8 0.00015 | 0.196 37.8 0.400 | 90.0 0.036 0.438 | |
| CALCULATION OF MANIFOLD FLOW | SPECIFIED OPIFICE DIAMETERS | SUPPLY AT UPIFICE 4 | NUMBER DE ERTETCES DRIFICE SPROING DISCHREGE COGEFFICIENT | MANIFOLD LEMSTH MANIFOLD AREA MANIFOLD HYTPAULIC DIA POUGHNESS | APEA BATIO LENGTH/DIAMETER RATIO K | AIR TEMPERATURE AIR VISCOSITY PRESOVET OR WATER | |

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| E PER E | 0.000 0.100 4.000 0.000 0.000 0.000 | |
| F F F | 0000 0000 0000 0000 0000 | |
| AIP DEN (SLUGASTS) | \$200 \$200 \$200 \$300 \$300 \$300 \$300 \$300 | |
| 6.00 0.00 0.00 | 0.444 0.0044 6.0044 0.004 | |
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TOTAL ATR FLOW

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| F FACT REY NO. | 0,0215 0,552E 05 0,0190 0,120E 05 0,0180 0,181E 06 0,0174 0,241E 06 | |
|-----------------------|--|----------|
| և. և. | | |
| AIR DEN (SLUG>FT3) | 0.00847 0.00347 0.00347 0.00346 | |
| я 60 С | 0.444 00.40 40.04 00.04 00.00 | |
| 19 (184) | က်က္ကက္ လက္လယ္ နေနာက္လ ကြလ္လ | 1 SCFM |
| | 1.0000 1.12855 1.0941 1.0694 | 1227.01 |
| 00 (00F0) | 40000 6000 6000 9000 9000 9000 9000 | P:07 |
| V1 (FPS) | പനധസ നേനവം നെപ്പുന് എന്നുന് | AIP FLOW |
| 11 : | e 00 연 ਚ | TOTAL |

| T REY NO | 08 0.6798 85 0.1468 76 0.0018 71 0.0018 | |
|---|--|---------------|
| I. L | 0.0203 0.0185 0.0176 0.0171 | |
| AIR DEN (SLUG/FT3) | 0,000 0,000 0,000 0,000 0,000 0,000 | |
| P3 (P31) | 0.44 0.14 0.01 0.00 0.00 0.00 0.00 | |
| 95 13 | | SCFM |
| OB NGPMAL | 1.0000 1.1433 1.1183 | 1507.13 |
| 50 (000 (000 (000 (000 (000 (000 (000 (| | Ē |
| V1 (FPS) | 14. 30.30 46.00 61.63 | HOTH RIB FLOW |
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| HL RIP FLDW | | ###################################### | | :- .u | 他の出版 ののにの 立のです。 中のです。 このでの立 | |
| VI 03 03 PI P3 SS.94 9.8831 1.1602 10.304 4.030 SS.94 9.8831 1.1602 10.304 4.030 SS.94 9.8831 1.1602 10.303 4.160 SS.11 9.4656 1.1345 10.203 4.160 HL RIP FLOW 2223.45 SCFM 4.30 VI 03 03 PI P3 VI 08 9.1392 1.0000 11.343 3.813 41.06 10.4528 1.1394 11.270 4.630 SS.91 10.5072 1.1394 11.270 4.641 | | \$ 10 0 0 0 \$ 10 0 0 0 \$ 2 0 0 \$ 5 0 0 0 | | | 00000 00140 2020 2020 2020 | |
| VI 03 NUPMBL (PSI) (PCI) 18.02 8.3453 1.0000 10.344 3.812 38.94 9.8531 1.1502 10.390 4.030 59.62 9.514 1.1456 10.308 4.150 59.62 9.514 1.1342 10.208 4.150 FPS (CES) NUPMBL (PSI) (PSI) 18.42 9.1392 1.0000 11.345 3.813 18.42 9.1392 1.1629 11.363 4.630 59.91 10.5072 1.1639 11.363 4.630 69.91 10.5072 1.1394 11.270 4.540 | AIP DEN MBC BIA | 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | | AIR DEN CLUGZETS: | | |
| FEST (305 03 PT) 18.02 8.3453 1.0000 10.94 38.94 9.8531 1.1502 10.33 59.62 9.7514 1.1455 10.36 88.11 9.4555 1.1345 10.88 PL RIP FLDW (2223.45 ST) 18.42 9.1392 1.0000 11.34 41.05 10.5072 1.1539 11.35 62.91 10.5072 1.1394 11.27 | | 00 4 4 4 00 4 00 4 00 4 00 00 00 00 4 | | <u></u> | 0444 0.2 (0.2 (0.0 0.4 0.0 0.1 | |
| PESS CORSY N CORSY N CERS CORS CORS CORS CORS CORS CORS CORS CO | 14. 15. | 110 110 110 110 110 110 110 110 110 110 | Ö Ö | P1 (P31) | 111 0.000 00 | (-) (-) |
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| | 315 89.5368 SETURE SET 2.93 | PAL HIP FLOW 2652.93 TOPM PAL HIP FLOW THEN NO. 19 19 19 19 19 19 19 19 19 19 19 19 19 | Feb. 618 Figure 03 Ft F3 Ft F57 NG. 1878 FFRCT F57 NG. 1888 FFRCT F57 NG. 1878 FFRCT F57 |

TABLE B-3 AFT MANIFOLD, 6-FOOT ORIFICE SPACING, ORIFICES NO. 5-8

| 57 575 575 | | | FT | 71 08 41 08 14 14 14 14 14 14 14 14 14 14 14 14 14 | | DEGREES P SLUGS/AT-SEC+10000 PSI/AT |
|------------------------------|-----------------------------|---------------------|--|--|------------------------------------|--|
| FLOE | SHE | | 400 00 01 . c | 18.0 87.7 8.0 6.00 0.00 15 | და ლაგა მა მა მა მა | က ကြောင့် စကာ ကြောင့် ကြောင့် ကြောင့် ကြောင့် ကြောင့် |
| CALCULATION OF MAMIFOLD FLOW | OPECIFIED CRIFICE DIRECTERS | CURPLY AT OPIFICE 4 | NUMBES OF BRITICES DRIFICE SPACING DISCHARGE COSFFICIENT | MANYFOLD LENGTE MANJFOLD AREA MANJFOLD HYPPOLIO DIA FOUGHHESS | Appa pajid Leusja Njamersp PPII | AIP VINCESTUPE AIP VINCESTIY PERMINET OF WHIER |

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| 55 144 217 | 9.000 0.00 0.400 40.000 | | in P | ##################################### | |
| E (1) (1) (1) | 0000 0000 0000 0000 0000 0000 0000 | | E G G U | 100 K H 60 K H 6 | |
| RIF DER (SLUG/FT2) | | | HIR DON (SLUGARIS) | | |
| (C) (C) (C) (C) | 位するの (0 m d (0 (0 m 2) (0 (0 m 2) (0 (0 m 2) (0 | | er € © © | 00 4 7 . 00 44 0 . 00 44 0 . 00 40 0 . 00 40 0 0 | |
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| 0 60 60 60 | 01-1 01-02- 01-02-0 01-02-0 01-02-0 | FLOW | SEC SCE SCE SCE SCE SCE SCE SCE SCE SCE | 00 0 0 0 00 0 0 0 00 0 0 0 00 0 0 0 0 0 0 0 | Ē, |
| VI (FPS) | 0.04. 0.04. 0.044 | я я 1 | ्र सम्ब | ស្រុកមស្ ១៤-១ ១៤-១ ១៤-១ ១០-១ | AIR FL |
| ĒĒ | स्कृतिक स | 10Tec | B | +4.0 (00 *) | TOTAL |

| 18. 19. | V1 (FPS) | os SCFS | OO NDAMBL | 191 100 100 | Po Pol U | AIR DEN ((LUG/FT3) | F FACT | REY MO. |
|------------------|------------------------------|--|--------------------------------------|--|---------------------------------------|--|--|--|
| 0, 0) rt | ადის თღათ თღ⊶თ საზა | 4 N.N.N. K.W.H.H. A.W.A.C. W.W.A.C. W.W.W.C. | 1.0000 1.1178 1.0032 1.0594 | 0.446 0.000 0.000 0.000 0.000 0.000 | დ գգ գ Ծ⊶մյո Խ⊶գգ ԾԾՇ | 0.00847 0.00847 0.00847 0.00847 | 0.00.000 0.0100 0.0100 0.0130 | 0.5608 05 0.1148 06 0.150E 06 0.2406 06 |
| TOTAL | AIP FLOW | 79.0 | 1222.14 | ⊗ B B B B B B B B B B B B B B B B B B B | | | | |
| 90 100 100 | V1 GPPS | 00 00 00 00 00 00 00 00 00 00 00 00 00 | 03 MOPMPL | P1 (PSI) | ⊕ ⊕ ⊕ ⊕ | AIP DEN (SLUG/FI3) | F FACT | REY MO. |
| स्थ⊙च | 4000 4000 4000 4000 | 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0 | 1.0000 1.1353 1.1106 | | 0444 0444 0449 0449 0440 | 0.00364 0.00364 0.00364 0.00364 | 0.0208 0.0185 0.0175 0.0171 | 0.600E 05 0.145E 06 0.221E 06 0.225E 06 |
| TOTAL | E I | FLOW | 1503.39 | WHO: | | | | |

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| संबंध का ख संबंध के जिल्ला संबंध के जिल्ला | | | BIR DEN CLUGAFT3) | 0.000000000000000000000000000000000000 | |
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| OO NDRAHL | © 90 P= Po © 30 Y0 90 © 97 01 +4 © +4 +4 +4 ****************************** | 1787.50 | 1644014 000 | 1.000 1.11 0.0000 0.000 000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0. | 1995.19 |
| 00 00 00 00 00 | ጭምምም መመው የመቀመ የመቀመ የመመመ የመመመ | 60.14 | 03 (SCES) | 0,000 0,000 0,000 0,000 0,000 0,000 | FLER |
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| | ਜ <i>ਹ</i> ੁ (ਹ ਤ | 15TH. | 1 . E | செற்றை | TOTAL |

| | 8830 | | • | တ္တတ္တ တက္ကတ္တ | |
|-----------------------|--|-------------|---------------------|--|---------|
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| F FRC1 | 0000 0000 0000 0000 0000 0000 | | я ТЭВСТ | 00.00 00.00 00.00 00.00 | |
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TABLE B-4 ALTERNATE FORWARD MANIFOLD, 42-FOOT ORIFICE SPACING

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| | V1 (FPS) | # 00 00 00 00 00 00 00 00 00 00 00 00 00 | AIP FLOW | V1 GP8⊝ | ###################################### |
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| n n G | ကေတက္ကတ္တင္ မေရာရာကို လူလင္ မေရာရာရာရက္က ကိုက်က်တိုက်တိုင်း | | (**) (**) (**) (**) (**) (**) (**) (**) | <u>.</u> |
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TABLE B-5 ALTERNATE AFT MANIFOLD, 4½-FOOT ORIFICE SPACING, ORIFICES NO. 1-5

CALCULATION OF MANIFOLD FLOW

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NUMBER DF DRIFICES

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| F FRCT | 00000 0000 0000 0000 0000 0000 0000 0000 | | H FROT | 00000 00000 00000 00000 |
| AIR DEN (SLUGYFT3) | 44.400 44.400 60.000 60.000 60.000 60.000 | | AIR DEF | ကြာသည် များသည် တို့သည် လိုင်းသည် တို့သည် လိုင်းသည် တို့သည် လိုင်းသည် တို့သည် လိုင်းသည် |
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| F РАСТ | 0.0801 0.0180 0.0178 0.0167 | | ғ ғ А СТ | 0000 0000 0000 0000 0000 0000 | |
| AIR DEN (SLUGZFI3) | 0.00413 0.00412 0.00412 0.00412 0.00412 | | AIR DEN (SLUG/FT3) | 00000 00000 00000 00000 444444 000000 000000 | |
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| OS NDFMAL | 0.000 0.000 0.000 0.000 0.000 | 0 † . 6388 | OB MORMAL | 000000 00000 00000 00000 00000 00000 0000 | 0000 10000 |
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| # E | स्थलच्छ | тотни | 20 H | ল এলেবিক | TOTEL |
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| PEY MO. | 0.981E 0.2814E 0.388E 0.441E 0.588E 0.587E | | REY MO. | 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 |
|-----------------------|--|---------------------------|-----------------------|---|
| F FACT R | 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 | | n FBC₹ | 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 |
| AIR DEN (SLUGZET3) | 0.00.00.00.00.00.00.00.00.00.00.00.00.0 | | AIR DEN (SLUGZFI3) | 0.00.00.00.00.00.00.00.00.00.00.00.00.0 |
| ₽3 104 | 0.0444 0.0400 0.0400 0.0000 0.0000 | | P3 (PSI) | დდ444 Γ Γ.ω.παα Γ.ω.παα Φ.Φ.Φ.ΔΑ |
| P1 (P31) | 011 011 010 00 00 00 00 00 00 00 00 00 0 | £ € ₩ | P1 (PCI) | |
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TOTHE PIP FLOW

TABLE 8-6 ALTERNATE AFT MANIFOLD, 4½-FOOT ORIFICE SPACING, ORIFICES NO. 6-10

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LOCATION 1 IS IN MANIFOLD REPROBABING DRINICE LOCATION 2 IS IN MANIFOLD ICANSTRESM OF CRIMICE LOCATION 3 IS DUISINE OF SRIFICE

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| V1 (FPS) | 6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 |
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TOTAL AIR PLOW 931

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148LE B-6 (continued)

| | V1 (FPS) | 03 (30FS) | OS NGRMAL | 91 (PSI) | 83 831 | HIR DEM (SLUGZETS) | F FACT | REY MD. |
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| | V1 FPS | 89 ୧୯୮୬ | OS MOPMAL | P1 (PSI) | 88 USB | AIR DEN (SLUG/FT3) | F FACT | REY NO. |
| | +00000 +00004 +0004 +00000 | 400000 60440 60460 64060 64460 | 000000 000000 000000 00000 | VVI-VV 000000 000000 | 04444 04000 44440 000000 | 0,000,00 0,000,00 0,000,00 0,000,00 0,000,00 0,000,00 0,000,00 | 0.02130 0.0130 0.0174 0.0174 | 0.000 0.1000 0.1000 0.0000 0.000 0.000 0.000 0.000 0.000 |
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| AIP DEN (SLUG/FT3) | 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | | PIP DEN (SLUG/FI3) | N. (2. (2. (2. (2. (2. (2. (2. (2. (2. (2 | |
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| . PEY 110. | 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0 | |
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| F FRCT | 0.0291 0.0128 0.0178 0.0178 0.0167 | |
| ALUGZETS) | 0,00413 0,00413 0,00413 0,00413 0,00412 | |
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| OO NORMAL | 0.4440 0.4440 0.4440 0.4440 |
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